

[DOCUMENT] SPECIFICATION
[TITLE OF THE INVENTION] OPTICAL ENCODER
[TECHNICAL FIELD]
[0001]

5 The present invention relates to an optical encoder,
which can optically detect a relative displacement between
gratings.

[BACKGROUND]
[0002]

10 In the non-patent document 1 noted below, proposed is
a theory of grating image (triplet grating method) in an
optical encoder provided with three gratings. According to
this theory, in case of using a spatially incoherent light
source, when a first grating, a second grating and a third
15 grating are arranged along a light propagating direction in
a particular condition, a predetermined spatial frequency
component, which is included in the first grating, can be
imaged on the third grating with a predetermined OTF
(Optical Transfer Function). The particular condition may
20 be defined by parameters, such as shape of the second
grating, a distance from the first grating to the second
grating, a distance from the second grating to the third
grating, etc. These parameters can define OTF of
respective spatial frequency components included in the
25 first grating to the third grating.

[0003]

In the theory of grating image (triplet grating
method), the respective three gratings have such functions
as: 1) the first grating; which defines a distribution of
30 spatial frequency on an incident plane, 2) the second

grating; OTF of each spatial frequency from the first grating to the third grating is defined by a shape of the second grating for applying transmittance modulation or phase modulation, a distance from the first grating to the second grating,
5 a distance from the second grating to the third grating, etc, 3) the third grating; which transmits only a desired component out of a distribution of imaging intensity, i.e., acts as an index slit.

10 [0004]

Meanwhile, in the following patent document 1, disclosed is an optical encoder for applications of the theory of grating image (triplet grating method). This optical encoder is composed of an optical transparent
15 grating as the first grating, which can create a light and dark pattern due to optical interference caused by difference in phase of light passing through the grating element, thereby reducing light cut off by the first grating. Consequently, more light can be transmitted to a
20 light-receiving element.

[0005]

[PATENT DOCUMENT 1] JP-10-2761(1998), A (Fig. 3)

[NON-PATENT DOCUMENT 1] K. Hane and C. P. Grover, "Imaging with rectangular transmission gratings," J. Opt. Soc. Am.

25 A4 706-711, 1987

[0006]

The optical encoder according to the patent document 1 employs a grating having opaque portions and transparent portions alternately arranged as the second grating, hence
30 OTF in the theory of grating image (triplet grating method)

is decreased. In addition, since the first transparent grating is irradiated with a diffusing light source to create the light and dark pattern due to optical interference caused by difference in phase of light, the contrast of the distribution of intensity, that is, the contrast of a spatial frequency component residing in the distribution of intensity on the incident plane is decreased.

[DISCLOSURE OF THE INVENTION]

10 [PROBLEM TO BE SOLVED BY THE INVENTION]

[0007]

An object of the present invention is to provide an optical encoder which can enhance OTF from a light source to a light receiving element and greatly improve efficiency of utilizing light.

[MEANS FOR SOLVING THE PROBLEM]

[0008]

An optical encoder according to the present invention includes: a light source; a first grating, which is composed of an amplitude grating having a first grating period, for spatial amplitude modulation of light from the light source; a second grating, which is composed of a phase grating having a second grating period, for spatial phase modulation of light from the first grating; a third grating, which is composed of an amplitude grating having a third grating period, for spatial amplitude modulation of light from the second grating; and a light receiving element for receiving light of the third grating, wherein the encoder detects a relative displacement between the respective gratings.

[0009]

It is preferable in the present invention that the second grating is composed of a transparent phase grating having an indented shape with a duty ratio of substantially
5 50%, in which optical path difference between the ridge and the valley thereof is substantially equal to $\lambda/2$ where λ is wavelength of light.

[0010]

Further, it is preferable in the present invention
10 that the second grating is composed of a transparent phase grating having an indented shape with a duty ratio of substantially 50%, in which optical path difference between the ridge and the valley thereof is substantially equal to $\lambda/4$ where λ is wavelength of light.

15 [0011]

In addition, it is preferable in the present invention that the second grating is composed of a reflective phase grating, and the first and third gratings are arranged on the same side with respect to the second grating.

20 [0012]

Further, it is preferable in the present invention that the second reflective grating has an indented shape with a duty ratio of substantially 50%, in which optical path difference between the ridge and the valley thereof is
25 substantially equal to $\lambda/4$, where λ is wavelength of light.

[0013]

Furthermore, it is preferable in the present invention that the second reflective grating has an indented shape with a duty ratio of substantially 50%, in which optical
30 path difference between the ridge and the valley thereof is

substantially equal to $\lambda/8$ where λ is wavelength of light.

[0014]

Moreover, it is preferable in the present invention that the first, the second and the third gratings have the same period P , and

both a first distance between the first and the second gratings and a second distance between the second and the third gratings are designed substantially to odd integral multiple of $P^2/(4\lambda)$ where λ is wavelength of light.

[0015]

Further, it is preferable in the present invention that the second grating has a period P , and the first and the third gratings have the same period $2P$, and

both a first distance between the first and the second gratings and a second distance between the second and the third gratings are designed to substantially odd integral multiple of $P^2/(4\lambda)$ where λ is wavelength of light.

[0016]

Furthermore, it is preferable in the present invention that the second grating is composed of a phase grating in which optical path difference varies sinusoidally.

[0017]

In addition, it is preferable in the present invention that a first distance Z_1 between the first and the second gratings is different from a second distance Z_2 between the second and the third gratings, and

the ratio of the first distance to the second distance is substantially equal to the ratio of a period of the first grating to a period of the third grating.

[0018]

Further, it is preferable in the present invention that the first, the second and the third gratings have scales of rotary type.

[0019]

5 Further, it is preferable in the present invention that the first grating has spatial distribution of transmittance varying sinusoidally.

[0020]

10 Furthermore, it is preferable in the present invention that a plurality of light receiving elements are arranged discretely with the third grating period, and the third grating and the light receiving elements are integrated with each other.

[EFFECT OF THE INVENTION]

15 [0021]

According to the present invention, employment of the second grating composed of a phase grating can enhance OTF according to the theory of grating image (triplet grating method), thereby greatly improving efficiency of utilizing light.

[BRIEF DESCRIPTION OF THE DRAWINGS]

[0022]

Fig. 1 is a schematic view showing Embodiment 1 according to the present invention.

25 Fig. 2 is a plan view showing an example of a grating pattern of a first grating.

Fig. 3 is a partial cross sectional view showing an example of a grating pattern of a second grating.

30 Fig. 4 is a graph showing relation of OTF to a distance between gratings, in case of optical path

difference on the second grating being $\lambda/2$, and $Z1 = Z2$.

Figs. 5A and 5B illustrate an example in case of using the second grating formed of a phase grating, in which Fig. 5a is a graph showing an example of an output signal from a light receiving element, and Fig. 5B is a graph showing a distortion component of the output signal.

Figs. 6A and 6B illustrate a comparative example in case of using the second grating formed of an amplitude grating, in which Fig. 6a is a graph showing an example of the output signal from the light receiving element, and Fig. 6B is a graph showing a distortion component of the output signal.

Figs. 7A and 7B illustrate an example in case of changing optical distances $Z1$ and $Z2$ in Embodiment 2 according to the present invention, in which Fig. 7a is a graph showing an example of the output signal from the light receiving element, and Fig. 7B is a graph showing a distortion component of the output signal.

Fig. 8 is a partial plan view showing another example of a grating pattern of a first grating in Embodiment 3 according to the present invention.

Figs. 9A and 9B illustrate an example in case of using the first grating shown in Fig. 8, in which Fig. 9a is a graph showing an example of the output signal from the light receiving element 17, and Fig. 9B is a graph showing a distortion component of the output signal.

Fig. 10 is a graph showing a calculation result of OTF in case of optical path difference on the second grating being $\lambda/4$, and $Z1 = Z2$.

Fig. 11 is a graph showing a calculation result of OTF

in case of changing the optical path difference (difference θ in phase) on the second grating in condition of $N = 2$.

Fig. 12 is a schematic view showing Embodiment 7 according to the present invention.

5 Fig. 13 is a graph showing a calculation result of OTF in condition of $N = 2$ and optical path difference being $\lambda/2$, in case of fixing the distance Z_1 and changing the distance Z_2 in a range of 0 to $2T$.

10 Fig. 14 is a graph showing relation between the distances Z_1 and Z_2 and periods P_1 and P_3 in imaging condition.

Fig. 15 is a schematic view showing Embodiment 8 according to the present invention.

15 Fig. 16 is a schematic view showing Embodiment 9 according to the present invention.

Fig. 17 is a schematic view showing Embodiment 10 according to the present invention.

Fig. 18 is a schematic view showing Embodiment 11 according to the present invention.

20 [EXPLANATORY NOTE]

[0023]

11	LIGHT SOURCE
12	FIRST GRATING
13, 15	SUBSTRATE
25 14	SECOND GRATING
16	THIRD GRATING
17	LIGHT RECEIVING ELEMENT
21, 71	TRANSPARENT AREA
22, 72	OPAQUE AREA

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[BEST EMBODIMENT FOR CARRYING OUT THE INVENTION]

[0024]

(Embodiment 1)

Fig. 1 is a schematic view showing Embodiment 1 according to the present invention. An optical encoder includes as components, along a light propagating direction, a light source 11, a first grating 12, a second grating 14, a third grating 16 and a light receiving element 17.

[0025]

10 The light source 11, which is composed of a spatially incoherent light source, such as LED, emits spatially incoherent light with central wavelength λ .

[0026]

15 The first grating 12, which is formed by patterning a metal thin film on a transparent substrate 13, constitutes an amplitude grating having a grating period P_1 so as to spatially amplitude-modulate the light from the light source. It is preferable that, as shown in a plan view of Fig. 2, a transparent area 21 and an opaque area 22 are alternately arranged at an interval of half of the grating period P_1 , i.e., $P_1/2$, to form an amplitude grating with a duty ratio of 50%.

[0027]

25 The second grating 14, which is formed by periodic binary level on the surface of a transparent substrate 15, constitutes a phase grating having a grating period P_2 so as to spatially phase-modulate the light from the first grating 12. It is preferable that, as shown in a cross sectional view of Fig. 3, the ridge and the valley thereof are alternately arranged at an interval of half of the

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grating period P_2 , i.e., $P_2/2$, to form a phase grating with a duty ratio of 50%. Further, it is preferable that optical path difference between the ridge and the valley is designed to substantially $\lambda/2$ (difference π in phase) where λ is wavelength of light. Hence, difference in phase between the light passing through the ridge and the light passing through the valley can be kept π , thereby maximizing OTF in the theory of grating image (triplet grating method).

10 [0028]

The third grating 16 constitutes an amplitude grating having a grating period P_3 so as to spatially amplitude-modulate the light from the second grating 14. It is preferable that, like the first grating 12 shown in Fig. 2, a transparent area and an opaque area are alternately arranged at an interval of half of the grating period P_3 , i.e., $P_3/2$, to form an amplitude grating with a duty ratio of 50%.

[0029]

20 The light receiving element 17, such as photo diode, converts the light passing through the third grating 16 into an electric signal. Herein the third grating 16 is located integrally onto a detecting surface of the light receiving element 17.

25 [0030]

The first grating 12 is secured to a housing or the like, and the third grating is secured to the light receiving element or the like, whereas the second grating 14 is supported movably along X-direction across the light propagating direction.

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[0031]

Here Z_1 is an optical distance from the first grating 12 to the second grating 14, and Z_2 is an optical distance from the second grating 14 to the third grating 16. In an illustrative case where P_1 , P_2 and P_3 are equal to each other and $Z_1 = Z_2$, to satisfy a condition that a spatial frequency component included in the first grating 12 can be imaged on the third grating 16, when the second grating 14 is displaced by half interval, i.e., $P_2/2$, of the grating period P_2 , distribution of light intensity on the third grating 16 moves by one interval. Then, the light passing through the third grating 16 is converted into an electric signal by the light receiving element 17, followed by counting changing of the signal intensity. Consequently, the relative displacement of the second grating 14 can be detected.

[0032]

Next, described below is a method for design of the condition that a spatial frequency component included in the first grating 12 can be imaged on the third grating 16, based on the theory of grating image (triplet grating method). In the example of Fig. 1, frequency property and contrast thereof of an image created on the third grating 16 can be obtained by calculating OTF (Optical Transfer Function). It is known that OTF can be expressed using Fourier transformation of the square of impulse response h as the following equation (1).

[0033]

[Equation 1]

$$F(\sigma_3) = \int |h(x_1, x_3)|^2 \exp(-2\pi i \sigma_3 x_3) dx_3 \quad (1)$$

where σ_3 ($= 1/P_3$) is a spatial frequency of the image on the third grating 16, and x_1 and x_2 are X-coordinates of the first grating 12 and the third grating 16 in Fig. 1, respectively.

[0034]

when calculating this OTF in a case of the second grating 14 having a periodic binary shape with a duty ratio of 50% and a optical path difference of $\lambda/2$ (difference π in phase), and $Z_1 = Z_2$, a result shown in Fig. 4 is obtained.

[0035]

In Fig. 4, the vertical axis means a relative output normalized by DC component, i.e., OTF, and the horizontal axis means the distance Z ($= Z_1 = Z_2$) normalized by Talbot position T , i.e., $(P_2)^2/\lambda$, which can be defined by wavelength λ and the period P_2 of the second grating 14. The letter N in Fig. 4 corresponds to parameter N in the imaging condition defined by the following equation (2).

[0036]

[Equation 2]

$$\left(1 + \frac{Z_2}{Z_1}\right) \times \sigma_3 \times P_2 = N \quad (2)$$

[0037]

In only case of this parameter N being an integer, a spatial frequency included in the first grating 12 can be imaged on the third grating 16 with a predetermined OTF. For example, in a case of $N = 2$, when each of distances Z_1 and Z_2 is an odd integral multiple of $T/4$, it can be imaged

on the third grating 16 with OTF of approximately 0.6. This OTF is comparable to double of the OTF value which has been described in the non-patent document 1 in case of using an amplitude grating as the second grating 14.

5 [0038]

Therefore, any combination of parameters, such as P_1 , P_2 , P_3 , Z_1 , Z_2 , λ , etc, can be selected for design so as to satisfy an imaging condition corresponding to parameter N in the above-described equation (2) and OTF in Fig. 4.

10 [0039]

For a specific example, the case of $N = 2$ with $P_1 = P_2 = P_3$ and $Z_1 = Z_2$ will be described below. Fig. 5A shows an output signal of the light receiving element 17, where $\lambda = 850$ nm; wavelength of the light source 11, $P_1 = 64.7$ μm ; grating period of the first grating 12, $P_2 = 64.7$ μm ; grating period of the second grating 14, $P_3 = 64.7$ μm ; grating period of the third grating 16, and $Z_1 = Z_2 = 1,230$ μm , i.e., $N = 2$. The vertical axis means signal intensity (arbitrary unit), and the horizontal axis means position of the second grating 14 (arbitrary unit). $Z_1 = Z_2 = 1,230$ μm are distances of $T/4$, corresponding to the position with the maximum OTF in the condition of $N = 2$ in Fig. 4. Incidentally, Fig. 5B is a graph showing a distortion component of the output signal, which may be an error factor for phase detection.

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[0040]

For a comparative example, Fig. 6A shows an output signal of the light receiving element 17, in the same condition of the first and third gratings 12 and 16 and the optical distances Z_1 and Z_2 and wavelength λ except for

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usage of an amplitude grating for the second grating 14. The vertical axis means signal intensity (arbitrary unit), and the horizontal axis means position of the second grating 14 (arbitrary unit). This amplitude grating has a transparent area and an opaque area being arranged alternately at an interval of $P2/2$, with a grating period of $P2$ ($= 64.7 \mu\text{m}$) and a duty ratio of 50%. Fig. 6B is a graph showing a distortion component of the output signal. [0041]

Comparing Fig. 5A to Fig. 6A, an output signal with a period of $32.35 \mu\text{m}$, that is half of the period $P2$ of the second grating 14, can be seen in each graph. But contrast of the signal exhibits 17% in Fig. 6A, whereas 38% with a good waveform in Fig. 5A. Incidentally, the contrast of intensity distribution on the third grating 16, which can be calculated based on the resultant output of the light receiving element, exhibits approximately 60% in Fig. 5A because of the duty ratio of the third grating 16 being 50%. This coincides generally with the calculation result of OTF shown in Fig. 4.

[0042]

Thus, employment of the second grating composed of a phase grating can improve OTF twice as much as an amplitude grating, and enhance contrast of the output signal from the light receiving element. In addition, such a phase grating can increase amount of light passing therethrough twice as much as the amplitude grating having a transparent area and an opaque area being repeated with a duty ratio of 50%, thereby improving efficiency of utilizing light emitted from the light source.

[0043]

In the above-described example, the optical distances Z1 and Z2 are designed to $T/4 = 1,230 \mu\text{m}$. In the case of the three grating periods P1, P2 and P3 being equal to each other, it can be seen from the result of Fig. 4 that OTF is maximized when each of the optical distances Z1 and Z2 is designed to odd integral multiple of $T/4$. Hence, in the above-described example, similar result can be attained when each of the optical distances Z1 and Z2 is designed to odd integral multiple of $T/4$. Moreover, even in the other case of Z1 and Z2 being not odd integral multiple of $T/4$, efficiency of utilizing light can be improved and contrast can be enhanced as shown in Fig. 4.

[0044]

15 (Embodiment 2)

In this embodiment, an optical encoder includes, along a light propagating direction, a light source 11, a first grating 12, a second grating 14, a third grating 16 and a light receiving element 17. This embodiment is configured similarly to Embodiment 1, but optical distances Z1 and Z2 are different from those of Embodiment 1.

[0045]

Specifically, in Embodiment 1, the optical distances Z1 and Z2 are designed to $1,230 \mu\text{m}$ or odd integral multiple thereof, respectively, in condition of $N = 2$. In this embodiment, the optical distances Z1 and Z2 are designed to $1,050 \mu\text{m}$, respectively, in condition of $N = 2$.

[0046]

Fig. 7a is a graph showing an output signal from the light receiving element in this embodiment, and Fig. 7B is

a graph showing a distortion component of the output signal. Each horizontal axis means position of the second grating 14 (arbitrary unit). The vertical axis of Fig. 7A means signal intensity (arbitrary unit). The vertical axis of Fig. 7B means distortion component, indicating an error between the output signal and an ideal sinusoidal waveform, that is further normalized by a peak-to-peak value.

[0047]

It can be seen that Fig. 7B exhibits slight variations of offset due to changing of observed distribution of light intensity, but a third order harmonic component is further reduced in comparison with the distortion component in the cases of using the phase grating and the amplitude grating shown in Figs. 5B and 6B.

[0048]

Moreover, contrast of the signal exhibits 36% with a good waveform in Fig. 7A, which is approximately equal to that of Fig. 5A.

[0049]

Here the reason why the third order harmonic component is reduced will be described below. In the above-described example, the first grating 12 is composed of an amplitude grating with rectangular distribution of transmittance, having a grating period P_1 and a duty ration of 50%. When the distribution of transmittance is resolved in spatial frequency using Fourier series, it can be expressed as the sum of a fundamental frequency component and odd order harmonic components, that is, a fundamental frequency component of the grating period P_1 , a third order harmonic component of threefold frequency, a fifth order harmonic

component of fivefold frequency, and so on.

[0050]

The theory of grating image (triplet grating method) defines OTF at every spatial frequency. Hence harmonic
5 components included in the first grating can be imaged on the third grating, depending on an imaging condition.

[0051]

Comparing Embodiment 2 with Embodiment 1, there is a difference in that changing of optical distances between
10 gratings alters OTF of harmonic components. In particular, Embodiment 1 is adjusted so as to maximize OTF of the fundamental frequency component while leaving OTF of harmonic components non-zero. Meanwhile, Embodiment 2 is designed so that OTF of harmonic components may approach
15 zero as small as possible in order to suppress the distortion component of the signal, while OTF of the fundamental frequency component is slightly lowered.

[0052]

As described above, appropriate adjustment of the
20 optical distances Z1 and Z2 using the theory of grating image (triplet grating method) can greatly reduce the distortion component residing in the output waveform, even when employing the first grating 12 of such an amplitude grating with rectangular distribution of transmittance as
25 shown in Fig. 2.

[0053]

In the above-described example, the optical distances Z1 and Z2 are designed to 1,050 μm . Any other condition can suppress unnecessary frequency components with the same
30 result.

[0054]

(Embodiment 3)

In this embodiment, an optical encoder includes, along a light propagating direction, a light source 11, a first grating 12, a second grating 14, a third grating 16 and a light receiving element 17. This embodiment is configured similarly to Embodiment 1, but distribution of transmittance of the first grating 12 is different from that of Embodiment 1.

[0055]

Specifically, Embodiments 1 and 2 employ the first grating 12 composed of an amplitude grating with rectangular distribution of transmittance, having a grating period P_1 and a duty ration of 50%. This embodiment employs the first grating 12 composed of an amplitude grating with sinusoidal distribution of transmittance, having a grating period P_1 .

[0056]

Fig. 8 is a partial plan view showing another example of the first grating 12. The first grating 12 is composed so that a plurality of gratings each having a sinusoidal spatial shape with the grating period P_1 , that is, a fundamental spatial frequency, are arranged in line. An opaque area 32 of the grating is defined between two sinusoids each having a reversed phase, and the opening width of a transparent area 31 varies sinusoidally along X-direction. When a beam of light having a predetermined sectional area enters the first grating 12, it is spatially amplitude-modulated sinusoidally to generate light having sinusoidal distribution of intensity.

[0057]

The second grating 14, like as the above-described embodiment, is composed of a phase grating with a duty ratio of 50%, in which the ridge and the valley thereof are alternately arranged at an interval of half of the grating period P_2 , i.e., $P_2/2$, so as to spatially phase-modulate the light from the first grating 12.

[0058]

The third grating 16, like as the above-described embodiment, is composed of an amplitude grating with a duty ratio of 50%, in which the transparent area and the opaque area thereof are alternately arranged at an interval of half of the grating period P_3 , i.e., $P_3/2$, so as to spatially amplitude-modulate the light from the second grating 14.

[0059]

For a specific example, Fig. 9A shows an output signal of the light receiving element 17, where $\lambda = 850$ nm, $P_1 = 64.7$ μm ; grating period of the first grating 12, $P_2 = 64.7$ μm ; grating period of the second grating 14, $P_3 = 64.7$ μm ; grating period of the third grating 16, and $Z_1 = Z_2 = 1,230$ μm (corresponding to positions with OTF being maximized in $N = 2$). The vertical axis means signal intensity (arbitrary unit), and the horizontal axis means position of the second grating 14 (arbitrary unit). Incidentally, Fig. 9B is a graph showing a distortion component of the output signal.

[0060]

Referring to these graphs, contrast of the signal exhibits 27%, which is slightly lowered as compared to the

case of using the first grating 12 having a rectangular opening, but no distortion component, such as third order harmonic component, takes place.

[0061]

5 Here the reason why no distortion component takes place when the transmittance of the first grating 12 varies sinusoidally at a fundamental frequency will be described below. According to the theory of grating image (triplet grating method), contrast of a spatial frequency component
10 on the third grating can be defined by each spatial frequency component on the first grating and OTF resulting from the second grating, the optical distances Z_1 and Z_2 and so on. In other words, when providing a grating which has no higher order components, i.e., whose transmittance
15 varies sinusoidally at a fundamental spatial frequency, as the first grating which may define distribution of spatial frequency on the incident plane, only the fundamental spatial frequency is always imaged on the third grating no matter how OTF of each harmonic component varies due to
20 error of the optical distances Z_1 and Z_2 .

[0062]

 Accordingly, by employing the first grating composed of an amplitude grating having sinusoidal distribution of transmittance, no higher harmonic component takes place in
25 principle. Even when the distance between gratings, such as Z_1 or Z_2 , varies, contrast of the signal slightly varies while the output signal including no higher harmonic component, i.e., distortion component, but the fundamental spatial frequency can be obtained.

30 [0063]

Incidentally, this embodiment exemplifies three sinusoidal gratings arranged as the first grating 12, as shown in Fig. 8. The number of gratings, constituting the transparent areas 31, may be one, two, four or more.

5 [0064]

(Embodiment 4)

In this embodiment, an optical encoder includes, along a light propagating direction, a light source 11, a first grating 12, a second grating 14, a third grating 16 and a
10 light receiving element 17. This embodiment is configured similarly to Embodiment 1, but height of the binary shape of the second grating 14 is different from that of Embodiment 1.

[0065]

15 Specifically, in Embodiment 1, optical path difference between the ridge and the valley of the second grating 14 is designed to $\lambda/2$ (difference π in phase). In this embodiment, the difference in optical path between the ridge and the valley of the second grating 14 is designed
20 to $\lambda/4$ (difference $\pi/2$ in phase). Similarly, the ridge and the valley are alternately arranged at an interval of half of the grating period $P2$, i.e., $P2/2$, to form a phase grating with a duty ratio of 50%.

[0066]

25 Fig. 10 is a graph showing a calculation result of OTF in case of optical path difference on the second grating 14 being $\lambda/4$, and $Z1 = Z2$. In Fig. 10, the vertical axis means a relative output normalized by DC component, i.e., OTF, and the horizontal axis means the distance Z ($= Z1 =$
30 $Z2$) normalized by Talbot position T , i.e., $(P2)^2/\lambda$, which

can be defined by wavelength λ and the period P_2 of the second grating 14. In order that a spatial frequency included in the first grating 12 can be imaged with a predetermined OTF on the third grating 16, any combination which satisfies both of the calculation result of OTF in Fig. 10 and the above-described imaging condition with respect to N can be selected, thereby allowing any combination of period of each grating, distance Z , etc. [0067]

10 For a specific example in a case of $N = 1$, when P_3 is double P_2 and each of the distances Z_1 and Z_2 is odd integral multiple of T according the equation of imaging condition, an image with OTF of approximately 0.6 can be created on the third grating. In this case, P_1 is equal to 15 P_3 . The resultant OTF of approximately 0.6 is equivalent to the maximum OTF shown in Fig. 4.

[0068]

(Embodiment 5)

In this embodiment, an optical encoder includes, along 20 a light propagating direction, a light source 11, a first grating 12, a second grating 14, a third grating 16 and a light receiving element 17. This embodiment is configured similarly to Embodiment 1, but height of the binary shape of the second grating 14 is different from that of 25 Embodiments 1 and 4.

[0069]

Specifically, in Embodiment 1, optical path difference between the ridge and the valley of the second grating 14 is designed to $\lambda/2$ (difference π in phase). In Embodiment 30 4, optical path difference between the ridge and the valley

of the second grating 14 is designed to $\lambda/4$ (difference $\pi/2$ in phase). In this embodiment, the difference in optical path between the ridge and the valley of the second grating 14 is designed to another value other than $\lambda/2$ (difference π in phase) and $\lambda/4$ (difference $\pi/2$ in phase). Similarly, the ridge and the valley are alternately arranged at an interval of half of the grating period $P2$, i.e., $P2/2$, to form a phase grating with a duty ratio of 50%.

[0070]

Fig. 11 is a graph showing a calculation result of OTF in case of changing the optical path difference (difference θ in phase) on the second grating 14 in condition of $N = 2$. In Fig. 11, the vertical axis means a relative output normalized by DC component, i.e., OTF, and the horizontal axis means the distance Z ($= Z1 = Z2$) normalized by Talbot position T , i.e., $(P2)^2/\lambda$, which can be defined by wavelength λ and the period $P2$ of the second grating 14.

[0071]

In a case of the optical path difference being $3\lambda/8$ ($\theta=3\pi/4$), as shown in Fig. 11, OTF is slightly degraded as compared to the case of the optical path difference being $\lambda/2$ ($\theta=\pi$), but it exceeds the OTF (approximately 0.3) in the case of using the amplitude grating with $N = 2$. According to the imaging condition of N and the calculation result of OTF, a combination of the period, the distance and the optical path difference on the second grating 14 can enhance amount of light twice as much as the amplitude grating, with contrast being improved.

[0072]

(Embodiment 6)

In this embodiment, an optical encoder includes, along a light propagating direction, a light source 11, a first grating 12, a second grating 14, a third grating 16 and a light receiving element 17. This embodiment is configured similarly to Embodiment 1, but a phase grating having a periodic binary shape with a duty ratio (ratio of valley to grating period P2) of a value, such 40% or 30%, other than 50% is employed as the second grating 14. In addition, the optical path difference between the ridge and the valley of the second grating 14 is also designed to a value other than $\lambda/2$ (difference π in phase) and $\lambda/4$ (difference $\pi/2$ in phase).

[0073]

In this case, according to the imaging condition of N and OTF, a combination of the period, the distance, the duty ratio and the optical path difference on the second grating can enhance amount of light twice as much as the amplitude grating, with contrast being improved.

[0074]

(Embodiment 7)

Fig. 12 is a schematic view showing Embodiment 7 according to the present invention. In this embodiment, an optical encoder includes, along a light propagating direction, a light source 11, a first grating 12, a second grating 14, a third grating 16 and a light receiving element 17. This embodiment is configured similarly to Embodiment 1, but both of the distance Z1 from the first grating 12 to the second grating 14 and the distance Z2 from the second grating 14 to the third grating 16 are different from those of Embodiment 1.

[0075]

Fig. 13 is a graph showing a calculation result of OTF in condition of $N = 2$ and optical path difference being $\lambda/2$, in case of fixing the distance Z_1 at $0.8 \times T/4$, $0.9 \times T/4$, $T/4$, $1.4 \times T/4$, $2.3 \times T/4$, or $3.0 \times T/4$, and changing the distance Z_2 in a range of 0 to $2T$, where T is Talbot position, i.e., $(P_2)^2/\lambda$, which can be defined by wavelength λ and the period P_2 of the second grating 14.

[0076]

10 In the theory of grating image (triplet grating method), the image of the first grating may be scaled up or down based on the ratio of Z_1 to Z_2 , while satisfying the following equation (3).

[0077]

15 [Equation 3]

$$Z_2 \sigma_3 = Z_1 \sigma_1 \quad (3)$$

[0078]

For example, in a case of $Z_1 = 0.9 \times T/4$, as shown in Fig. 14, spatial frequencies $\sigma_3 (= 1/P_3)$ and $\sigma_1 (= 1/P_1)$ may vary depending on the ratio of Z_1 to Z_2 , that is, the period P_1 of the first grating 12 and the period p_3 of the third grating 16 may vary depending on the ratio of Z_1 to Z_2 .

[0079]

25 In a specific case of $\lambda = 850 \text{ nm}$, $P_2 = 64.7 \text{ }\mu\text{m}$, and $Z_1 = 1.1 \text{ mm}$, OTF is approximately 0.6 at $Z_2 = 2.2 \text{ mm}$ by reading Fig. 13, where $P_3 = 97.2 \text{ }\mu\text{m}$ and $P_1 = 48.6 \text{ }\mu\text{m}$ in Fig. 14. Therefore, the image of the first grating 12 having $48.6 \text{ }\mu\text{m}$ is scaled up twofold on the third grating 13.

30 [0080]

According to this configuration, the image on the third grating can be enlarged, thereby enhancing contrast and amount of light thereof, and advantageously facilitating alignment of the third grating.

5 [0081]

The above-described case exemplifies the optical path difference of $\lambda/2$, but any combination can constitute a scale-up or scale-down system whenever satisfying the imaging condition of OTF and N, and each condition of spatial frequency defined by the ratio of Z1 to Z2. In addition, even in another case of the optical path difference of, e.g., $\lambda/4$, other than $\lambda/2$, any combination can constitute a scale-up or scale-down system whenever satisfying the imaging condition of OTF and N, and each condition of spatial frequency defined by the ratio of Z1 to Z2.

[0082]

(Embodiment 8)

Fig. 15 is a schematic view showing Embodiment 8 according to the present invention. In this embodiment, an optical encoder includes, along a light propagating direction, a light source 11, a first grating 12, a second grating 14, a third grating 16 and a light receiving element 17. This embodiment is configured similarly to Embodiment 1, but a phase grating in which the optical path difference varies sinusoidally is employed as the second grating 14.

[0083]

In this case, like above, the image of the first grating 12 can be created on the third grating 16 by

combining design parameters, such as the period, the distance Z , based on the calculation result of OTF and the imaging condition.

[0084]

5 For example, in a case of $N = 1$ and the optical path difference between the top of the ridge and the bottom of the valley of the second grating 14 being $\lambda/4$ (difference $\pi/2$ in phase), OTF is approximately 0.6 at a position of $Z_1 = Z_2 = T$, thereby further improving contrast in comparison
10 with an amplitude grating, and doubling amount of light.

[0085]

 Fig. 15 shows as an example the second grating 14 composed of the phase grating having the optical path difference varies sinusoidally. But the second grating 14
15 may be composed of another phase grating having a periodic distribution of phase, such as triangular or stepwise waveforms, thereby doubling amount of light in comparison with an amplitude grating, and improving contrast.

[0086]

20 (Embodiment 9)

 Fig. 16 is a schematic view showing Embodiment 9 according to the present invention. For easy understanding, each above-described embodiment exemplifies a linear encoder including linear-shaped gratings. The present
25 invention can be applied to a rotary encoder including gratings which are arranged radially with a predetermined angular period.

[0087]

 In this embodiment, an optical encoder includes, along
30 a light propagating direction, a light source 11, a first

grating 12, a second grating 14, a third grating 16 and a light receiving element 17. The second grating 14 is supported angularly displaceable around a central axis C. [0088]

5 The light source 11, which is composed of a spatially incoherent light source, such as LED, emits spatially incoherent light with central wavelength λ . An optical axis Q of the light source 11 is located parallel to the central axis C and at a position of radius R_a from the
10 central axis C.
[0089]

 The first grating 12, which is formed by patterning a metal thin film on a transparent substrate 13, constitutes a rotary scale of an amplitude grating type having a
15 grating period P_1 at the position across the optical axis Q so as to spatially amplitude-modulate the light from the light source. It is preferable that, like as shown in Fig. 2, a transparent area 21 and an opaque area 22 are alternately arranged at an interval of half of the grating
20 period P_1 , i.e., $P_1/2$, to form a sector-shaped amplitude grating with a duty ratio of 50%.
[0090]

 The second grating 14 is formed by periodic binary level on the surface of a transparent disk-shaped substrate
25 15, which is rotatable around the central axis C. The second grating 14 constitutes a rotary scale of a phase grating type having a grating period P_2 at the position across the optical axis Q so as to spatially phase-modulate the light from the first grating 12. It is preferable
30 that, as shown in a cross sectional view of Fig. 3, the

ridge and the valley thereof are alternately arranged at an interval of half of the grating period P_2 , i.e., $P_2/2$, to form a sector-shaped phase grating with a duty ratio of 50%. Further, it is preferable that the optical path difference
5 between the ridge and the valley is designed to substantially $\lambda/2$ where λ is wavelength of light. Hence, difference in phase between the light passing through the ridge and the light passing through the valley can be kept π , thereby maximizing OTF in the theory of grating image
10 (triplet grating method).

[0091]

The third grating 16 constitutes a rotary scale of an amplitude grating type having a grating period P_3 at the position across the optical axis Q so as to spatially
15 amplitude-modulate the light from the second grating 14. It is preferable that, like the first grating 12 shown in Fig. 2, a transparent area and an opaque area are alternately arranged at an interval of half of the grating period P_3 , i.e., $P_3/2$, to form a sector-shaped amplitude
20 grating with a duty ratio of 50%.

[0092]

The light receiving element 17, such as photo diode, converts the light passing through the third grating 16 into an electric signal. Herein the third grating 16 is
25 located integrally onto a detecting surface of the light receiving element 17.

[0093]

The first grating 12 is secured to a housing or the like, and the third grating 16 is secured to the light
30 receiving element or the like, whereas the second grating

14 is supported to be angularly displaceable along a circumferential direction perpendicular to the optical axis Q.

[0094]

5 Here Z1 is an optical distance from the first grating 12 to the second grating 14, and Z2 is an optical distance from the second grating 14 to the third grating 16. OTF in the rotary encoder can be calculated by substituting the grating period in the above-described linear displacement
10 with the grating period at the position across the optical axis Q, to which the above-described theory of grating image (triplet grating method) can apply.

[0095]

15 In an illustrative case where $Z1 = Z2$ and $N = 2$ to satisfy a condition that a spatial frequency component included in the first grating 12 can be imaged on the third grating 16, when the second grating 14 is displaced by half interval, i.e., $P2/2$, of the grating period $P2$, distribution of light intensity on the third grating 16
20 moves by one interval. Then, the light passing through the third grating 16 is converted into an electric signal by the light receiving element 17, followed by counting changing of the signal intensity. Consequently, the relative displacement of the second grating 14 can be
25 detected.

[0096]

30 The above-described case exemplifies the optical path difference of $\lambda/2$, but any combination can constitute a rotary encoder whenever satisfying the imaging condition of OTF and N. In addition, even in another case of the

optical path difference of, e.g., $\lambda/4$, other than $\lambda/2$, any combination can constitute a rotary encoder whenever satisfying the imaging condition of OTF and N.

[0097]

5 (Embodiment 10)

Fig. 17 is a schematic view showing Embodiment 10 according to the present invention. For easy understanding, each above-described embodiment exemplifies a transparent phase grating for the second grating 14. The present
10 invention can be applied to a case of using a reflective phase grating for the second grating 14.

[0098]

In this embodiment, an optical encoder includes, along a light propagating direction, a light source 11, a first
15 grating 12, a second grating 14, a third grating 16 and a light receiving element 17, wherein the slit direction of each of the gratings 12, 14 and 16 is designed perpendicular to the sheet of the drawing, and the moving direction of the second grating 14 is designed as a top-to-
20 bottom direction, parallel to the sheet of the drawing. The light from the light source 11 passes obliquely through the first grating 12, and then reflects obliquely on the second grating 14, and then passes obliquely through the third grating 16, and then reaches the light receiving
25 element 17. Each of Z1 and Z2 is defined as a distance along the light propagating direction.

[0099]

The above-described theory of grating image (triplet grating method) also can apply to this case by substituting
30 the step of the second grating 14 with half of that of the

transparent phase grating. In a case of, for example, the optical path difference between the ridge and the valley of the transparent second grating 14 being $\lambda/2$ (difference π in phase), the optical path difference between the ridge and the valley of the reflective second grating 14 is $\lambda/4$ (difference $\pi/2$ in phase). In another case of the optical path difference between the ridge and the valley of the transparent second grating 14 being $\lambda/4$ (difference $\pi/2$ in phase), the optical path difference between the ridge and the valley of the reflective second grating 14 is $\lambda/8$ (difference $\pi/4$ in phase).

[0100]

Thus, by employment of such a reflective phase grating as the second grating 14, a set of the light source 11 and the first grating 12 and another set of the third grating 16 and the light receiving element 17 can be arranged on the same side with respect to the second grating 14, thereby attaining a compact configuration as a whole.

[0101]

(Embodiment 11)

Fig. 18 is a schematic view showing Embodiment 11 according to the present invention. This embodiment employs a reflective phase grating for the second grating 14. like the above embodiment. But the slit direction of each of the gratings 12, 14 and 16 is designed as a top-to-bottom direction, parallel to the sheet of the drawing, and the moving direction of the second grating 14 is designed perpendicular to the sheet of the drawing. The light from the light source 11 passes obliquely through the first grating 12, and then reflects obliquely on the second

grating 14, and then passes obliquely through the third grating 16, and then reaches the light receiving element 17. Each of Z1 and Z2 is defined as a distance along the light propagating direction.

5 [0102]

The above-described theory of grating image (triplet grating method) also can apply to this configuration. In addition, a set of the light source 11 and the first grating 12 and another set of the third grating 16 and the light receiving element 17 can be arranged on the same side with respect to the second grating 14, thereby attaining a compact configuration as a whole.

[0103]

In each embodiment described above, a case of the first grating 12 and the third grating 16 being fixed and the second grating 14 being movable is exemplified, but the second grating 14 may be fixed and the first grating 12 and the third grating 16 may be movable. Further, a system of the second grating 14 and the third grating 16 being moved relatively to the first grating 12 and another system of the first grating 12 and the second grating 14 being moved relatively to the third grating 16 can also obtain a signal.

[0104]

In each embodiment described above, a case of the first grating 12 being composed of a grating whose transmittance varies rectangularly or sinusoidally is exemplified, but the distribution of transmittance of the first grating 12 can be designed appropriately so as to realize a desired distribution of intensity (distribution of spatial frequency) on a subsequent imaging plane.

30

[0105]

In each embodiment described above, a case of the third grating 16 having a duty ratio of 50% is exemplified, but it may be other than 50%, and the distribution of transmittance of the third grating 16 can be designed appropriately so as to obtain a desired output.

[0106]

In each embodiment described above, a case of the third grating 16 being composed of light shielding slits is exemplified, but a plurality of light receiving elements, which correspond to a opening shape of the third grating 16, may be arranged discretely with the grating period P3 to sum outputs from the light receiving elements, thereby enabling integration of the third grating 16 and the light receiving element 17 to simplify assembling operation and reduce the number of parts.

[0107]

In each embodiment described above, anti-reflection coating may be applied onto each of light passing planes of the gratings 12, 14 and 16 to reduce loss of light. In this case, thickness of each coating is considered for optical design, in particular, difference in phase.

[0108]

In each embodiment described above, a case of light from the light source directly entering the first grating 12 is exemplified, but a light diffusing plate having a predetermined diffusion angle may be interposed between the light source 11 and the first grating 12 so that diffused light can enter the first grating 12. In this case, adjustment of the diffusion angle of the light diffusing

plate can reduce amount of light deviating out of the detecting area of the light receiving element 17, thereby improving efficiency of utilizing light.

[INDUSTRIAL APPLICABILITY]

5 [0109]

According to the present invention, OTF from the light source to the light receiving element can be enhanced and efficiency of utilizing light can be greatly improved, resulting in an optical encoder with high performance and a
10 compact size.